

## Implementing Different Boiling Models in the Development of FLUBOX-3D Code.

### INTRODUCTION

FLUBOX-3D is a computational fluid dynamics simulation tool for the accurate description of two-phase-flow conditions inside the reactor pressure vessel. It simulates multi-dimensional two-phase-flow of water and steam on basis of a two-fluid-model.

The subject of the present work is the implementation of multidimensional modeling of vertical upward subcooled boiling flow in FLUBOX-3D code using a two fluid approach and calculation of two phase flow void fraction.

### SUBCOOLED BOILING MODELS

The subcooled boiling is considered as a **combination of evaporation near wall and condensation in the bulk**, see Fig. 1

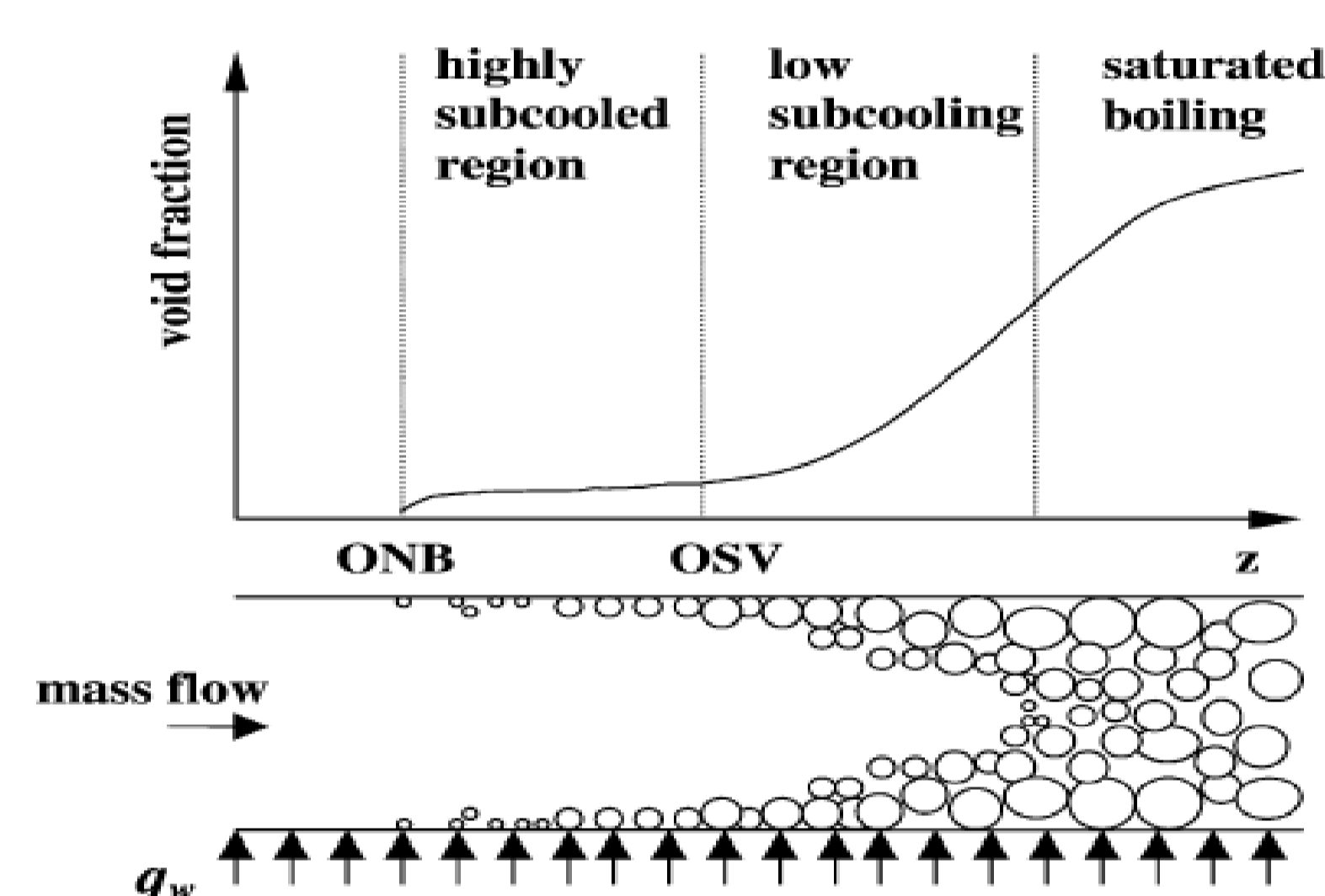


Figure 1 schematic description of the axial void fraction profile in the subcooled boiling regions for upward vertical flow

A set of two models for wall evaporation and another set of condensation models in the bulk were adopted to be implemented in the FLUBOX code

- Evaporation Models
  - lahey mechanistic model
  - Kurul and Podowski model
- Condensation Models
  - Ranz\_Marshall Nusselt number,
  - Hughmark correlation.
  - The modified Unal-Lahey correlation.

So for simplicity and to easily understand the figures of work validation, the models are divided in three main models, as follow:

- **Model 1:** Hughmark for condensation, and Kurul-Podowski for evaporation.
- **Model 2:** Unal-Lahey for condensation, and lahey mechanistic for evaporation.
- **Model 3:** Ranz-Marshall for condensation, and lahey mechanistic for evaporation.

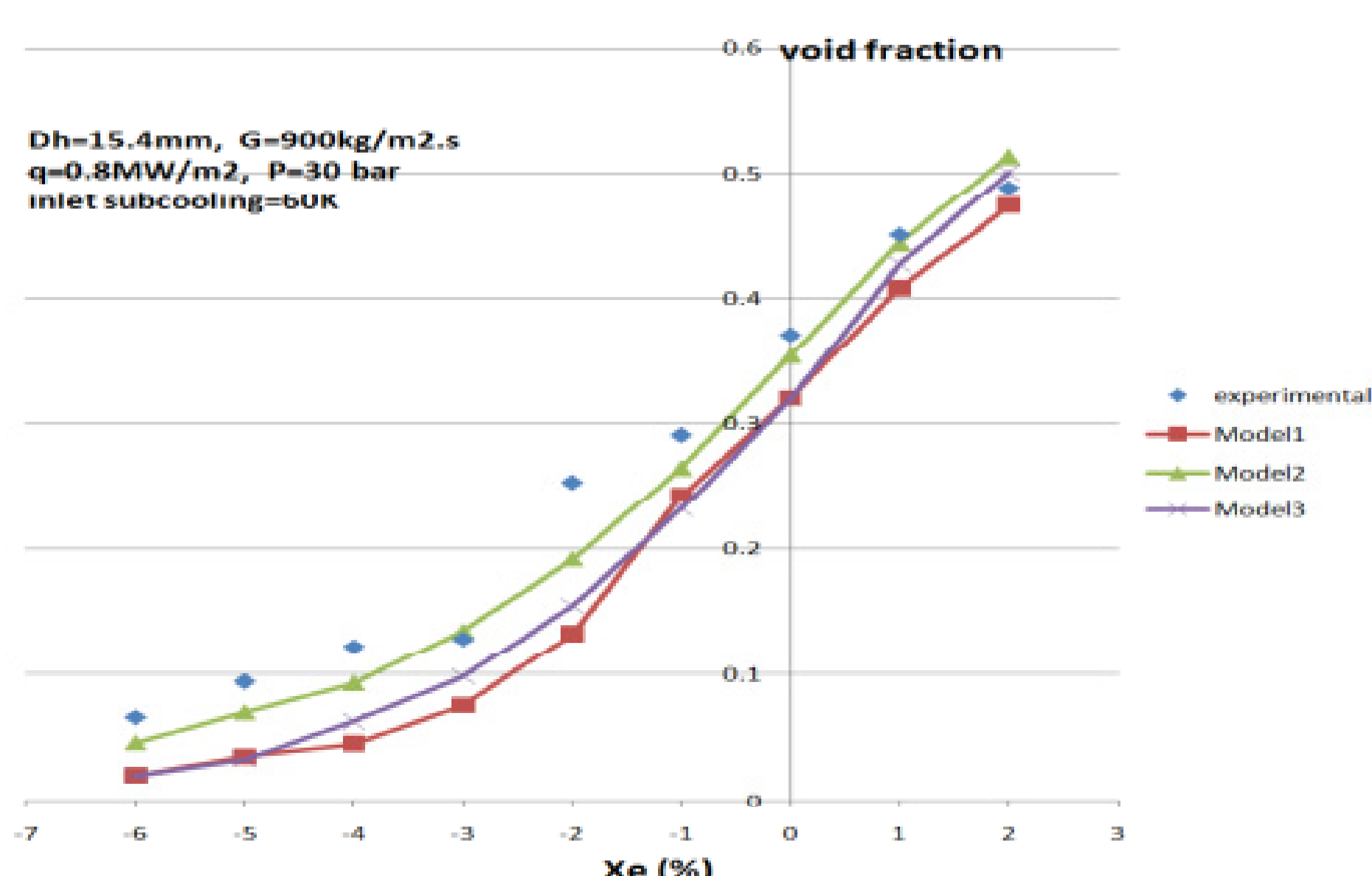


Figure 2 Thermodynamic quality versus void fraction. P=30 bar, q=0.8MW/m², Dh = 15.4mm

### VALIDATION OF THE MODELS

Bartolomej Experiment:

The Bartolomej experiment was performed in 2m long heated tube with an inner diameter of 15.4mm, a water pressure of 30 and 45 bar, heat flux (0.38; 0,8) MW/m² and mass flow velocity 900 Kg/m²s. The inlet temperature subcooling condition varied between 20 °C and 160 °C.

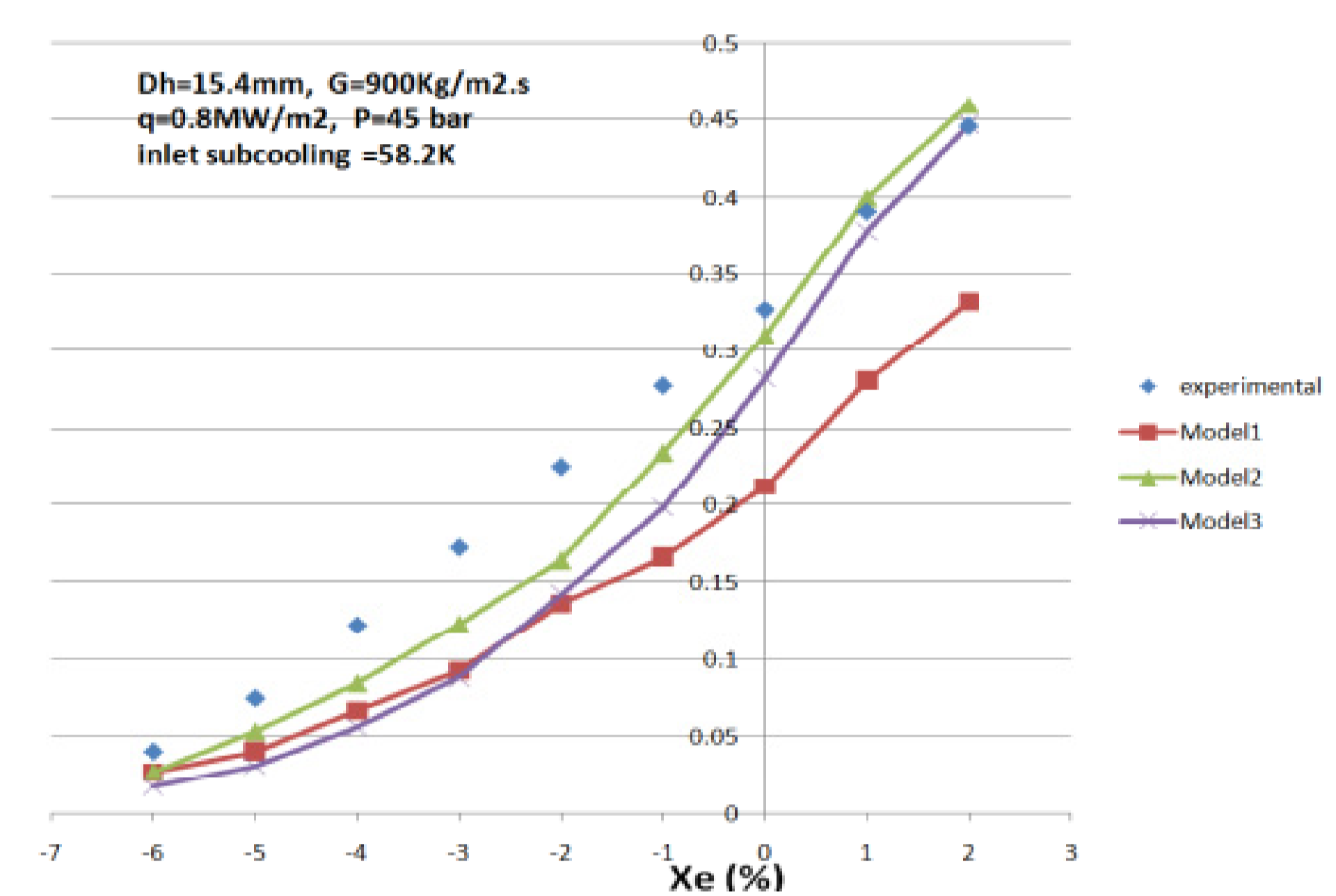


Figure 3 Thermodynamic quality versus void fraction. P=45 bar, q=0.8MW/m², Dh = 15.4 mm

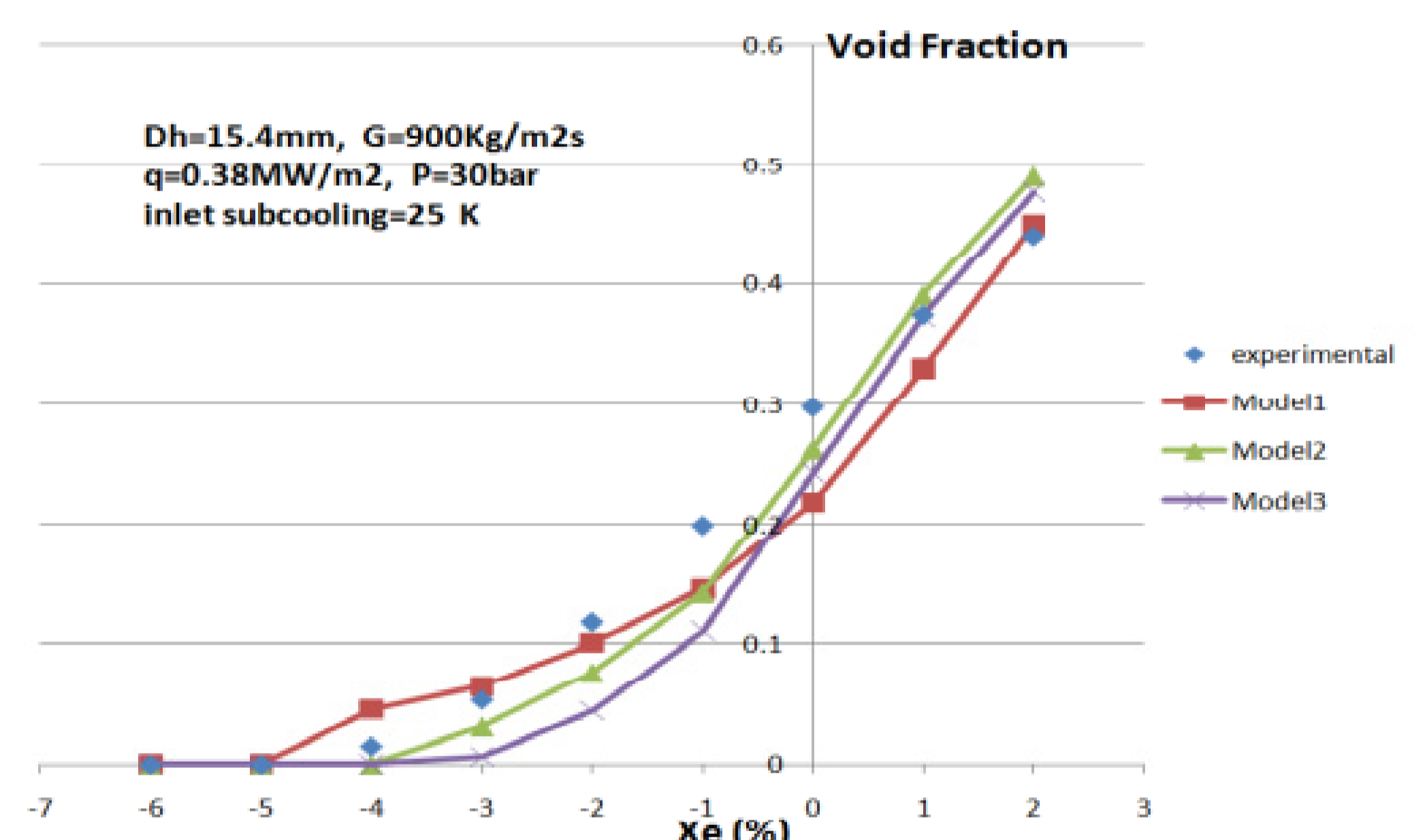


Figure 4 Thermodynamic quality versus void fraction. P=30 bar, q=0.38MW/m², Dh = 15.4 mm

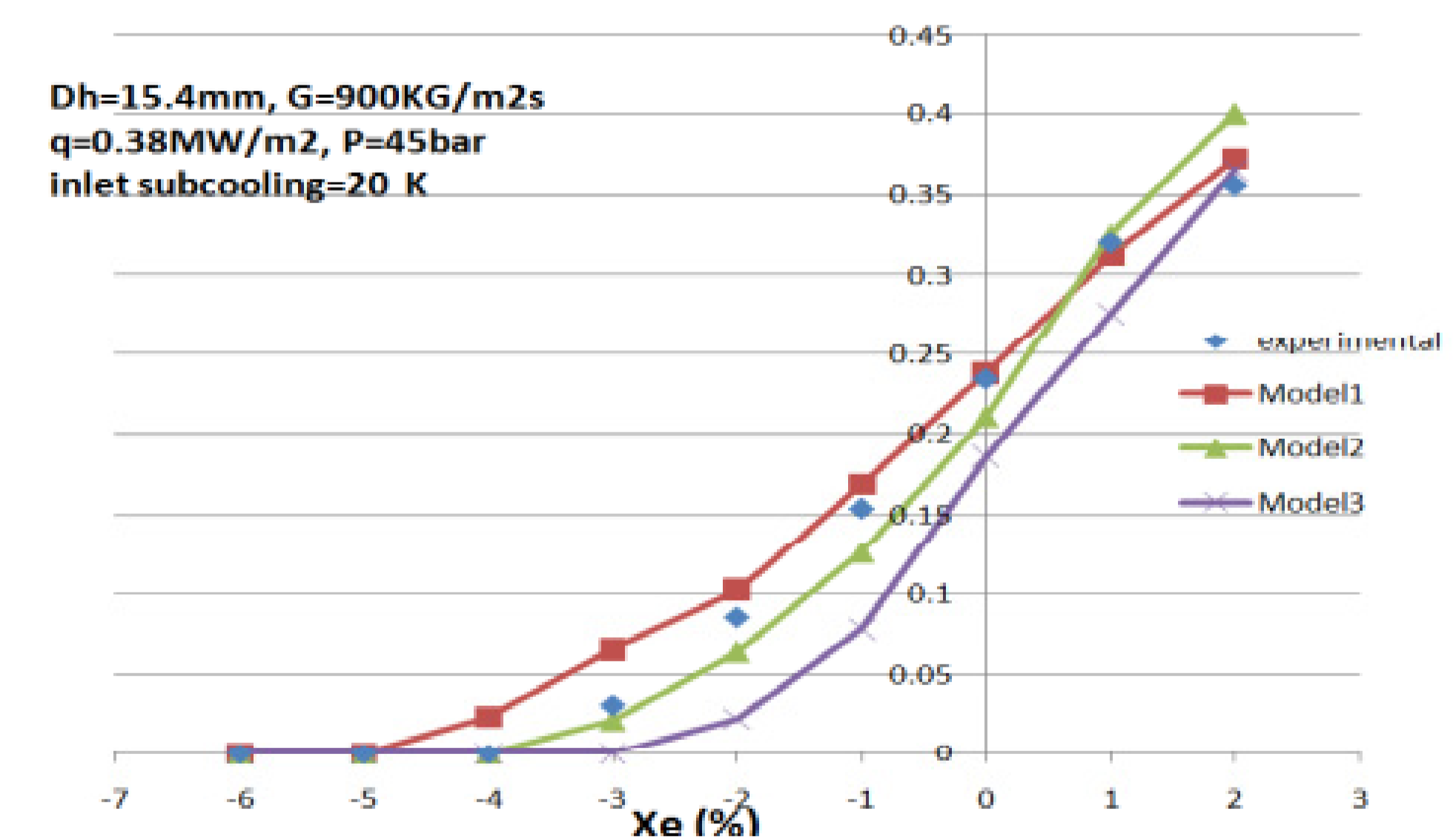


Figure 5 Thermodynamic quality versus void fraction. P=45 bar, q=0.38MW/m², Dh = 15.4 mm

### CONCLUSION

The results of the simulation indicate that the implemented **Model 2** which is a combination of modified **Unal-Lahey** model for condensation and **Lahey mechanistic** model for evaporation resulted in better void fraction prediction.

For further queries, please contact:  
[Abdullah.Alali@ntech.mw.tum.de](mailto:Abdullah.Alali@ntech.mw.tum.de) ; Tel. : 089 289 15624